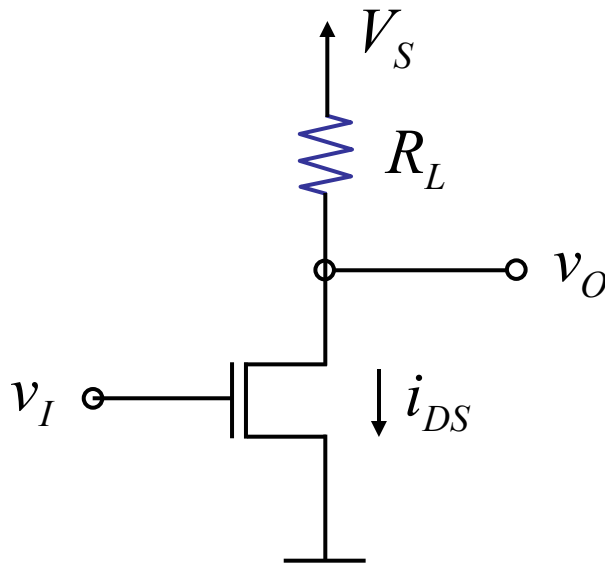


Amplifiers -- Small Signal Model

Review

■ MOSFET amp



■ Saturation discipline — operate MOSFET only in saturation region

■ Large signal analysis

1. Find v_O vs v_I under saturation discipline.
2. Valid v_I , v_O ranges under saturation discipline.

Reading: Small signal model -- Chapter 8

Large Signal Review

① v_O vs v_I

$$v_O = V_S - \frac{K}{2} (v_I - 1)^2 R_L$$

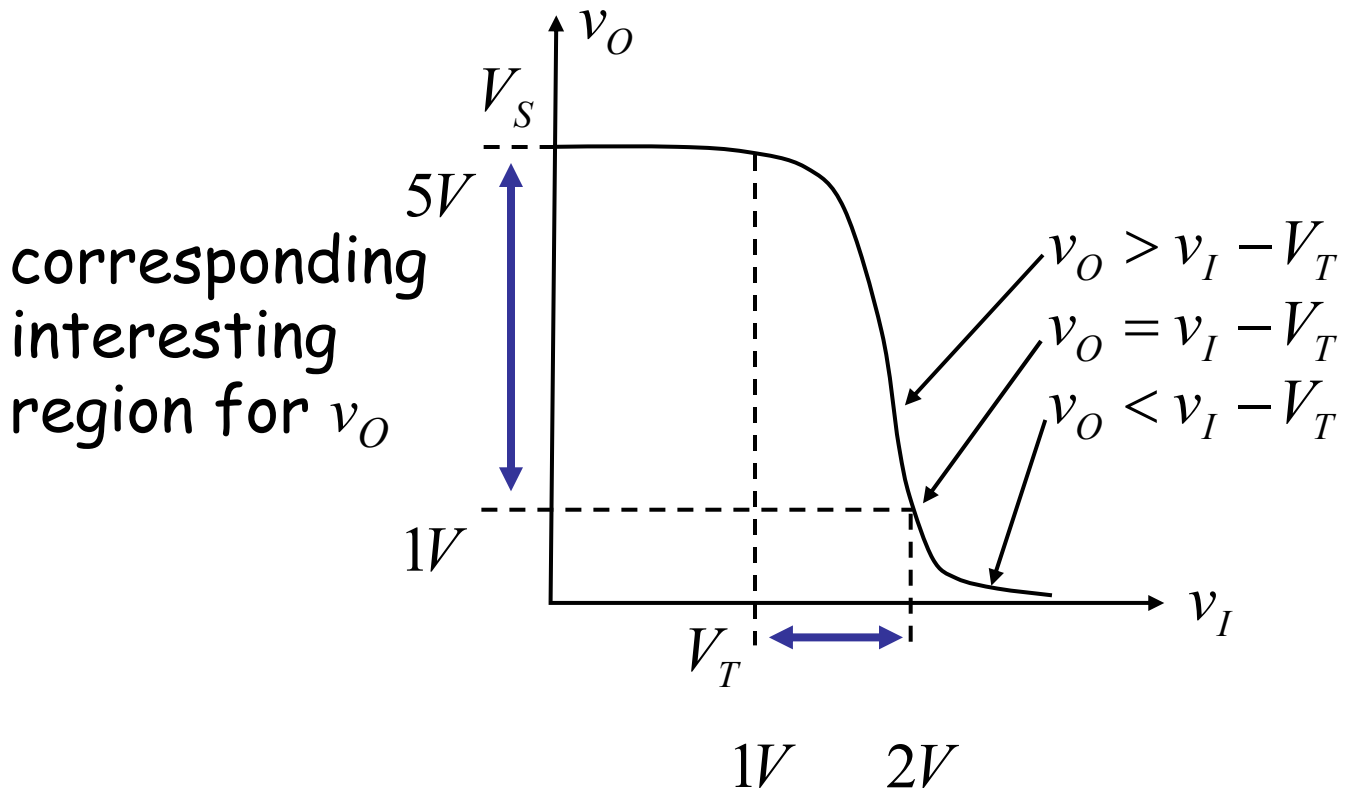
valid for $v_I \geq V_T$
and

$$v_O \geq v_I - V_T$$

(same as $i_{DS} \leq \frac{K}{2} v_O^2$)

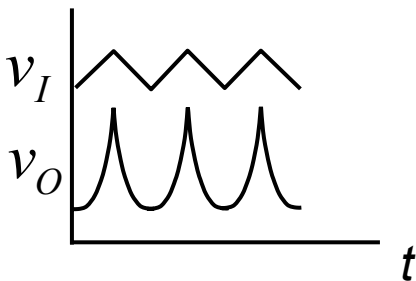
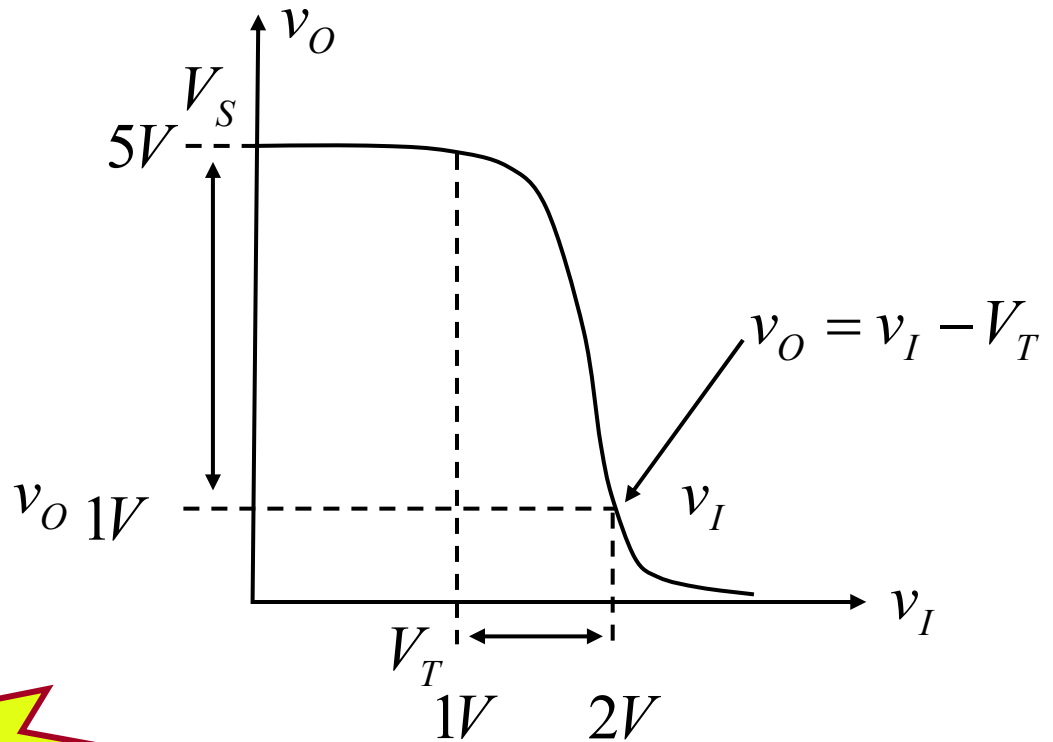
Large Signal Review

② Valid operating ranges



"interesting" region for v_I . Saturation discipline satisfied.

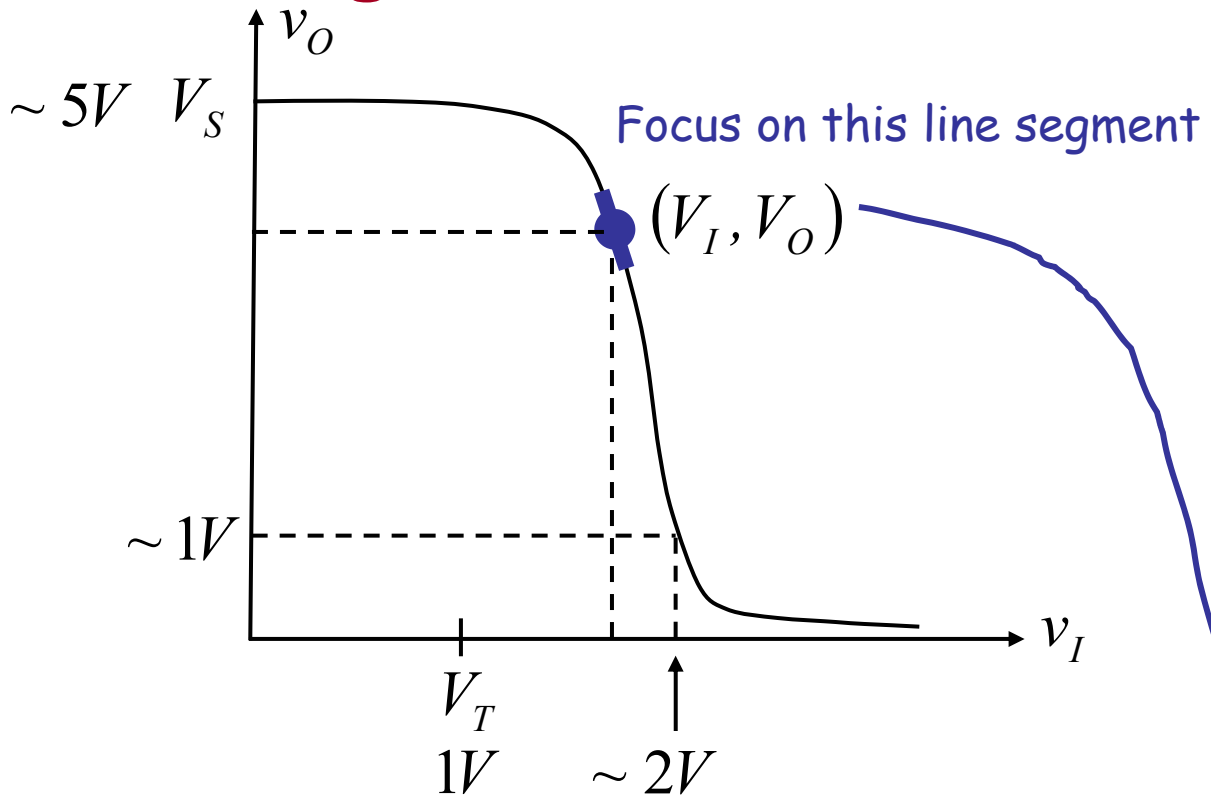
But...



Amplifies alright,
but distorts

Amp is nonlinear ... ☹️

Small Signal Model



$$v_O = V_S - \frac{K(v_I - V_T)^2}{2} R_L$$

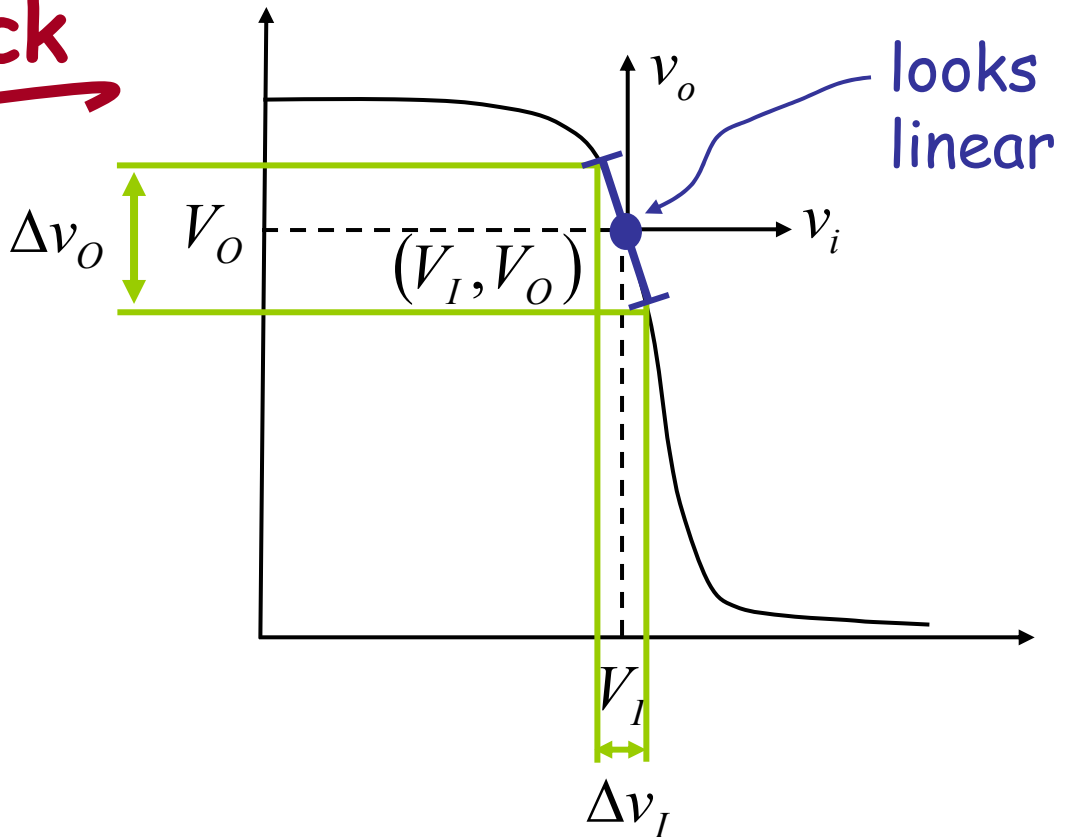
Amp all right, but nonlinear!

Hmmm ... So what about our linear amplifier ???

Insight:

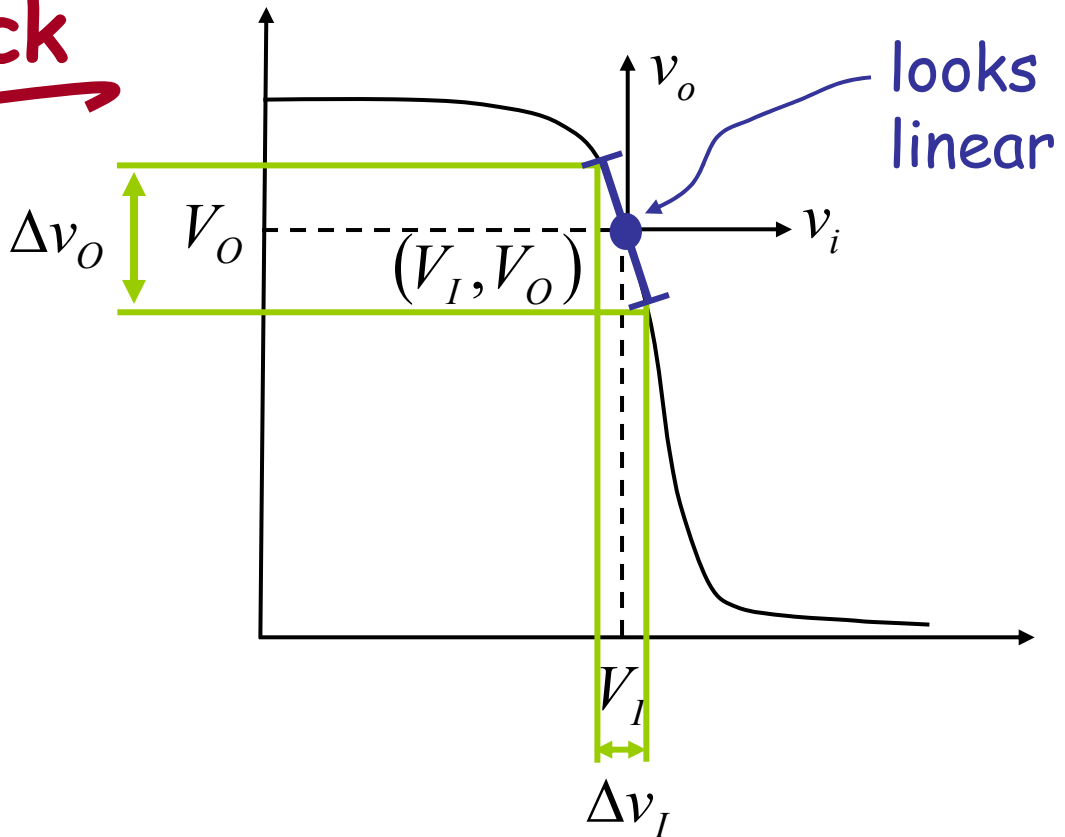
But, observe v_I vs v_O about some point (V_I, V_O) ... looks quite linear!

Trick



- ❖ Operate amp at V_I, V_O
→ DC "bias" (good choice: midpoint of input operating range)
- ❖ Superimpose small signal on top of V_I
- ❖ Response to small signal seems to be approximately linear

Trick



- ❖ Operate amp at V_I, V_O
→ DC "bias" (good choice: midpoint of input operating range)
- ❖ Superimpose small signal on top of V_I
- ❖ Response to small signal seems to be approximately linear

Let's look at this in more detail —

I graphically

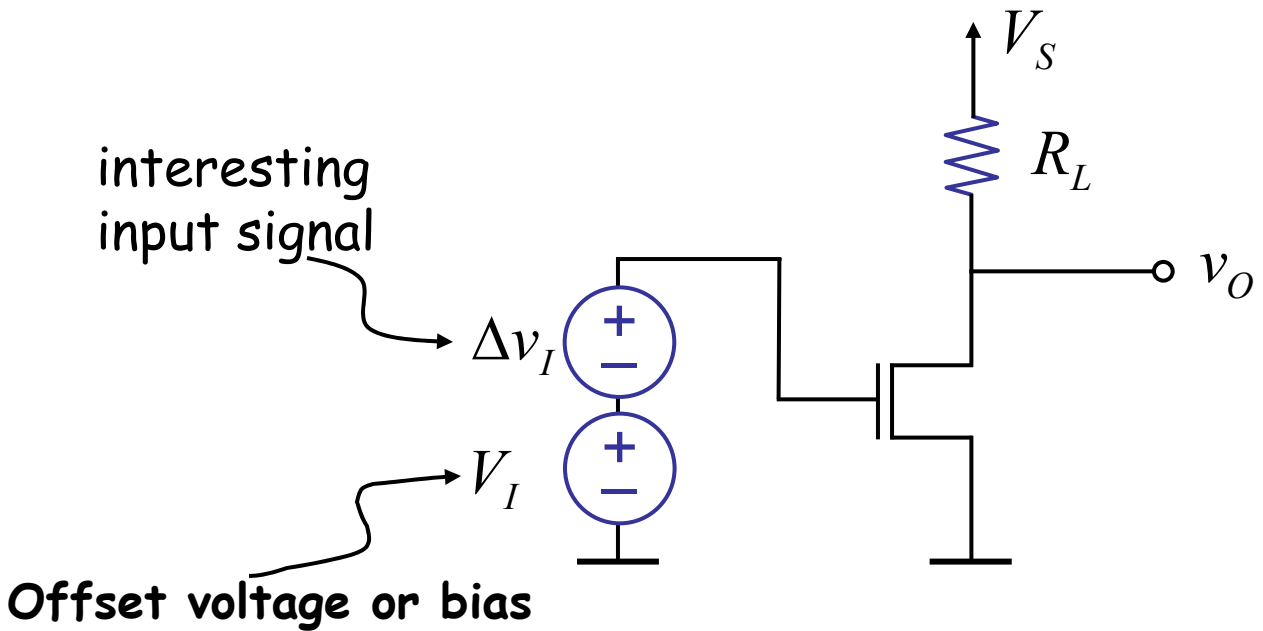
II mathematically

III from a circuit viewpoint

next week

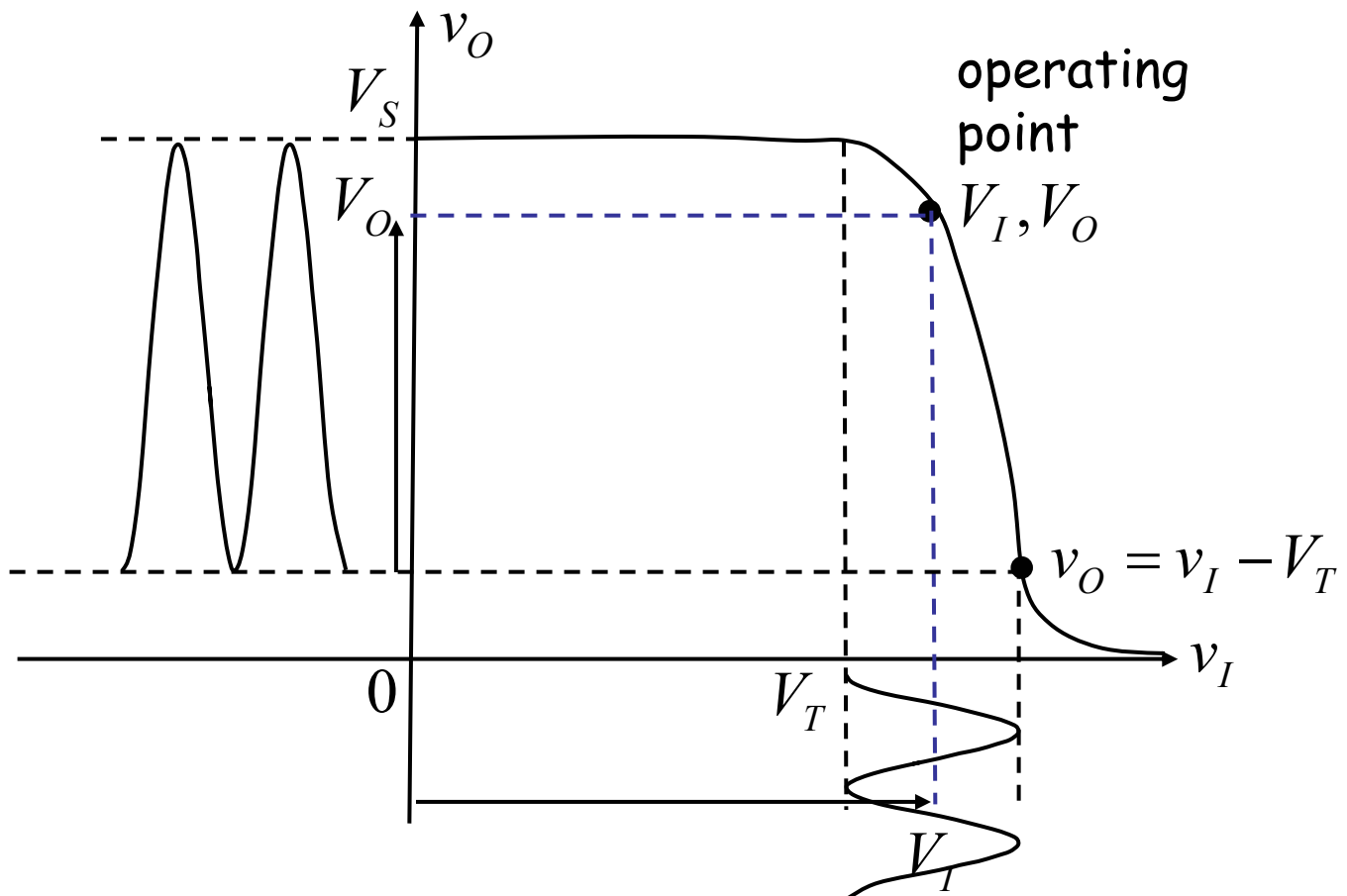
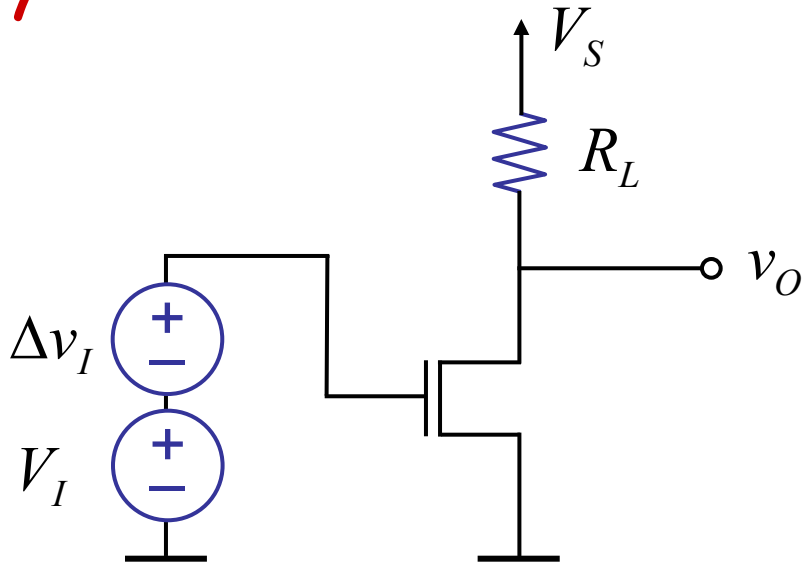
I Graphically

We use a DC bias V_I to “boost” interesting input signal above V_T , and in fact, well above V_T .



Graphically

interesting
input signal



Good choice for operating point:
midpoint of input operating range

Small Signal Model

aka incremental model

aka linearized model

Notation —

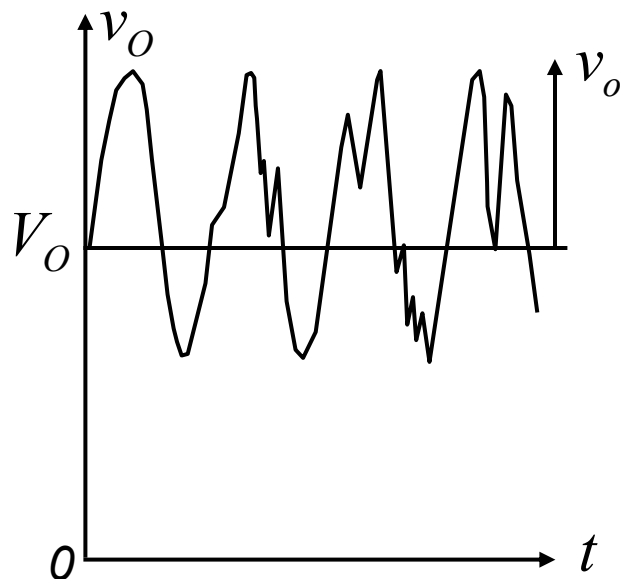
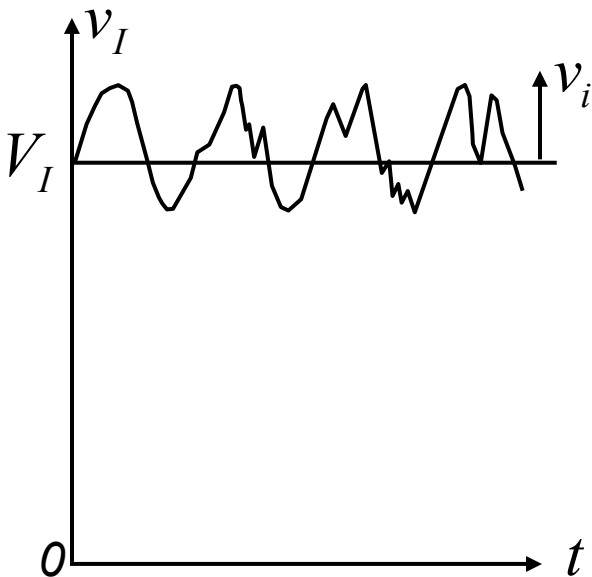
Input: $v_I = V_I + v_i$

total variable DC bias small signal (like Δv_I)

↓
bias voltage aka operating point voltage

Output: $v_O = V_O + v_o$

Graphically,



II Mathematically

(... watch my fingers)

$$v_O = V_S - \frac{R_L K}{2} (v_I - V_T)^2 \quad \Bigg| \quad V_O = V_S - \frac{R_L K}{2} (V_I - V_T)^2$$

substituting $v_I = V_I + v_i$ $v_i \ll V_I$

$$v_O = V_S - \frac{R_L K}{2} ([V_I + v_i] - V_T)^2$$

$$= V_S - \frac{R_L K}{2} ([V_I - V_T] + v_i)^2$$

$$= V_S - \frac{R_L K}{2} ([V_I - V_T]^2 + 2[V_I - V_T]v_i + v_i^2)$$

$$V_O + v_o = V_S - \frac{R_L K}{2} (V_I - V_T)^2 - R_L K (V_I - V_T) v_i$$

From \star ,

$$v_o = - \underbrace{R_L K (V_I - V_T)}_{g_m} v_i \quad \text{related to } V_I$$

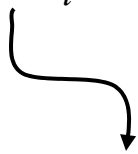
Mathematically

$$v_o = -R_L \underbrace{K (V_I - V_T)}_{g_m} v_i \quad \text{related to } V_I$$

$$v_o = -g_m R_L v_i$$

For a given DC operating point voltage V_I , $V_I - V_T$ is constant. So,

$$v_o = -A v_i$$


constant w.r.t. v_i

In other words, our circuit behaves like a linear amplifier for small signals

Another way

$$v_o = V_S - \frac{R_L K}{2} (v_I - V_T)^2$$

$$v_o = \underbrace{\frac{d}{dv_I} \left[V_S - \frac{R_L K}{2} (v_I - V_T)^2 \right]}_{\text{slope at } V_I} \bigg|_{v_I = V_I} \cdot v_i$$

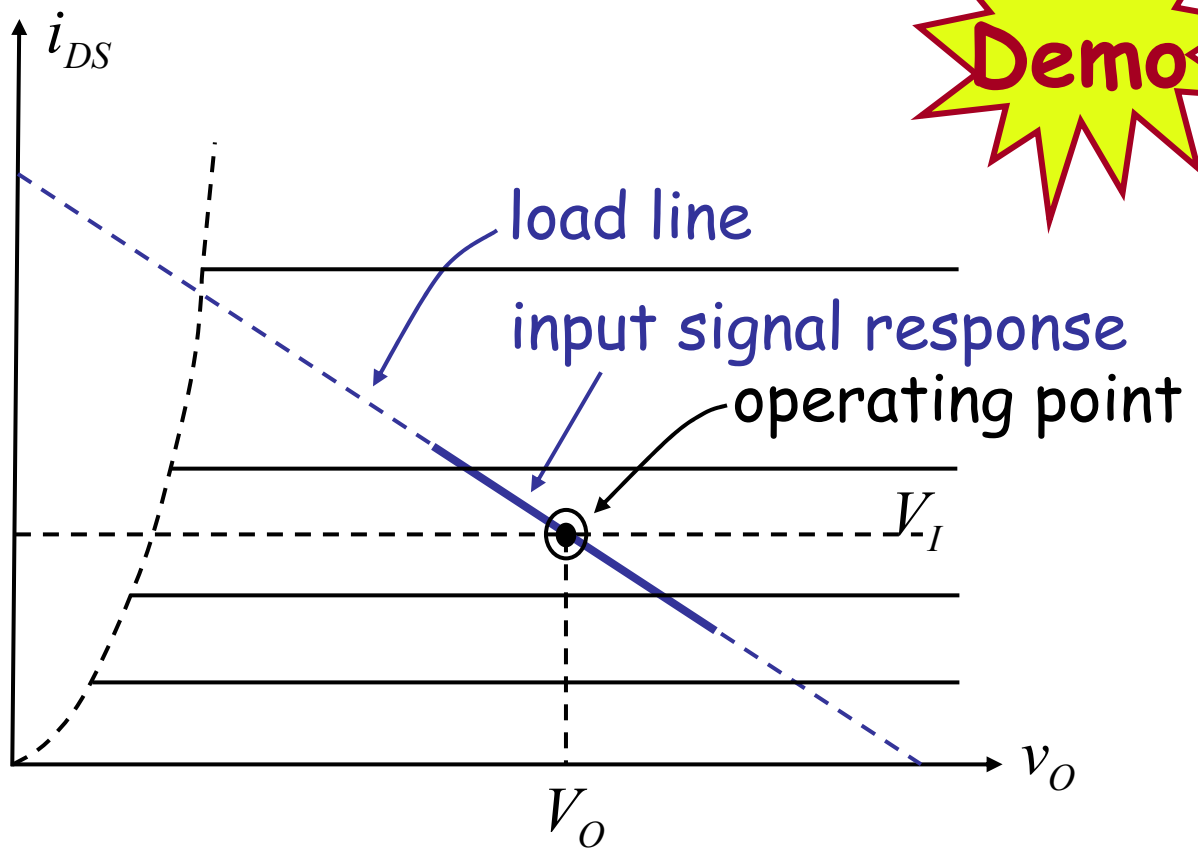
$$v_o = -R_L K (V_I - V_T) \cdot v_i$$

$$g_m = K (V_I - V_T)$$

$$A = -g_m R_L \quad \text{amp gain}$$

Also, see Figure 8.9 in the course notes
for a graphical interpretation of this result

More next lecture ...



How to choose the bias point:

1. Gain component $g_m \propto V_I$
2. v_i gets big \rightarrow distortion.
So bias carefully
3. Input valid operating range.
Bias at midpoint of input operating range for maximum swing.